RESOLUTION

JORDAN SCHOOL DISTRICT BOARD OF EDUCATION

Resolution of Appreciation to Legislators within Jordan District Boundaries and to the City Councils of Bluffdale, Herriman, Riverton, South Jordan and West Jordan.

Whereas, the Utah Legislature voted a four percent increase in the state education WPU and an additional two percent increase in education funding targeted at growth, and

Whereas, legislators within Jordan School District made every effort to support both portions of one of the largest funding increases for education in recent years, and

Whereas, the County-wide Equalization program for property taxes was originally designed to benefit Jordan School District when it split from Canyon School District, and

Whereas, said equalization program was due to expire in 2016 without specific instructions in the law for ending the program, and;

Whereas, the legislators and City Councils within Jordan School District boundaries recognized the serious financial shortfall facing the school district because of a lack of state code regarding a method for ending the county-wide property tax program, and

Whereas, local legislators and city officials worked together with the Jordan School District Board of Education to propose a solution to the sunset of the county equalization program which would allow the Jordan School District to access the property tax rate which had been in effect prior to the equalization program, and

Whereas, the efforts of those elected officials resulted in a change to the state code which will return property tax rates in Jordan School District to the level which had been approved by taxpayers as a result of a Truth-in-Taxation hearing after the school district split in 2009,

Therefore, Be It Hereby Resolved, that the Jordan School District Board of Education expresses its *Profound Appreciation* for the legislative support of Senators Wayne Harper, Aaron Osmond, and Howard Stephenson, and Legislators Kim Coleman, Richard Cunningham, Ken Ivory, John Knotwell, Dan McCay, and Earl Tanner, as well as the City Councils of Bluffdale, Herriman, Riverton, South Jordan, and West Jordan. It is the pleasure of the Jordan School District Board of Education to work with these, our locally elected officials, in behalf of all children enrolled in publicly funded schools, and it is our hope and our intent to continue that relationship with our elected officials to ensure the finest education possible for the children within the Jordan School District boundaries.

Adopted on this 31st day of March, 2015, by the Board of Education for Jordan School District, West Jordan, Utah.

Susan K. Pulsipher
Board President

Janice L. Voorhies
Board Vice President

Kayleen Whitelock
Board Secretary

Jen Atwood
Board Member

J. Lynn Crane
Board Member

Richard S. Osborn
Board Member

Matt Young
Board Member

RIVERTON CITY, UTAH
OFFICE OF THE MAYOR

A PROCLAMATION OF RIVERTON CITY MAYOR APPLEGARTH

WHEREAS, one in every 2,500 pregnancies are diagnosed with a congenital diaphragmatic hernia (CDH); and

WHEREAS, since 2000, it is estimated that over 500,000 babies have been born with CDH; however, only 50 percent of those babies survived; and

WHEREAS, CDH is as common as spina bifida and cystic fibrosis; however, very few people know about it or are aware of it; and

WHEREAS, 1,600 babies are born with CDH every year in the United States; and

WHEREAS, there are many people living in Utah who have been diagnosed with and have survived their CDH; although many families in Utah have endured the pain and grief associated with the loss of loved ones with CDH; and

WHEREAS, those with CDH often endure multiple surgeries and possible medical complications beyond their diagnosis that include heart defects, pulmonary complications, gastric and intestinal problems, as well as developmental delays, and they may require respiratory and medicinal support for years; and

WHEREAS, raising awareness of this congenital defect will help bring about acceptance and support for those suffering with it and will help advocate for urgently needed medical research and advances.

NOW THEREFORE, I, Bill Applegarth, Mayor of Riverton City, do hereby proclaim April 19 as a **Day of Congenital Diaphragmatic Hernia Awareness**.

GIVEN, with the Seal of Riverton City on this seventh day of April 2015.

[SEAL]

RIVERTON CITY INCORPORATED Seal 1947 STATE OF UTAH

Bill Applegarth, Mayor

Attest:

Virginia Loader, Recorder

S

CKR Engineers, Inc.
Consulting Structural Engineers

December 28, 2009

Mr. Brian Morrow
RhinoRock LLC
PO BOX 971178
Orem, Utah 84097

Re: 6 ft. RhinoRock Concrete Fence Testing

CKR File: 9536

Dear Brian:

This letter addresses the testing performed by RhinoRock LLC on the "RhinoRock" concrete fence panel. The "RhinoRock" panel measures 4-1/4 in. thick by 8 ft. - 4 in. wide by 6 ft. tall. The hollow panel consists of a thin fiber-reinforced concrete surface with strategically located composite ribs in the panel interior. See Photographs 1 to 4. For the complete fence system, the panels will be attached to precast concrete posts bearing on footings. This letter only addresses the load testing of the fence panel; it does not address the posts or footing system.

Panel Testing

1. CKR Engineers did not design the "RhinoRock" fence panel, nor have we performed a structural analysis of the panel. A total of 5 load tests were performed on the concrete panels. I observed the full test of panel #2. RhinoRock personnel performed and provided video records to our office of the other four tests.

2. The testing appears to have been completed in accordance with generally accepted materials engineering and testing principles and practices. No other warranty, either expressed or implied, is made by CKR Engineers. CKR Engineers is evaluating the information supplied by RhinoRock. RhinoRock takes responsibility for the testing data.

3. Each panel was tested by placing it horizontally and bearing the short ends on 6 in. wide continuous foam support pads. See Photograph 1. Approximately 4 to 5 in. of the panel was bearing on the foam. See Photographs 3 and 5. A 2x8 wood frame was placed on top of and around the perimeter of the panel for the first test. A plastic liner was placed inside the frame, and then the frame was slowly filled with water. For the remainder of the tests, a 2x4 wood frame was placed on top of the 2x8 frame to allow for more water depth. The panel in test #2 was loaded to failure. See Photograph 6. The other

remaining panels were not tested to failure. You showed me the panel used for test #1. There were no visible signs of cracking or distress in the panel after the test. You informed me that panels 3, 4 and 5 also did not show any signs of cracking or distress.

4. The following table summarizes the testing data.

Test	Average Depth of Water	Weight of Water	Weight of Panel*	Total Load	Tested to Failure
1	8 in.	42 psf	5 psf	47 psf	No
2	12 – ¾ in.	66 psf	5 psf	71 psf	Yes
3	9 – ¾ in.	50 psf	5 psf	55 psf	No
4	9 in.	46 psf	5 psf	51 psf	No
5	9 – ½ in.	49 psf	5 psf	53 psf	No

1. *Weight of panel supplied by RhinoRock personnel.

5. Based upon our evaluation of the supplied testing data, we recommend that the panel be limited to a maximum allowable wind pressure of 44 psf. This number is calculated by taking the 71 psf ultimate load from test #2 and dividing it by a factor of safety of 1.6.
6. This testing data recommendation is limited to the panel only. The suitability of this panel in a particular location to resist potential applied loads (wind, seismic, impact) should be evaluated by a qualified structural engineer. Care should be taken to insure that the panel is installed plumb, and properly attached to the concrete precast posts.

Fence Wind Pressures

The pressure imposed upon a fence by the wind is a function of the wind speed, exposure and aspect ratio of the fence. The 2006 *International Building Code* references the American Society of Civil Engineers document *ASCE 7-05 Minimum Design Loads for Buildings and Other Structures* for wind pressures. Included with this letter are calculations for a number of different wind speeds and exposures using the requirements of ASCE 7-05. It should be noted that wind pressures on a fence are higher at a free end of a fence than in an interior portion of the fence. The following table summarizes the calculated pressures.

Wind Speed	Exposure	End Pressure End to 6 ft	End Pressure 6 ft to 12 ft.	End Pressure 12 ft. to 18 ft.	Interior Pressure > 30 ft.
90 mph	B	25.8 psf	15.3 psf	11.7 psf	10.0 psf
100 mph	B	31.8 psf	18.9 psf	14.4 psf	12.0 psf
110 mph	B	38.5 psf	22.8 psf	17.5 psf	14.6 psf
120 mph	B	45.8 psf	27.2 psf	20.8 psf	17.3 psf
90 mph	C	38.1 psf	22.6 psf	17.3 psf	14.4 psf
100 mph	C	47.0 psf	27.9 psf	21.3 psf	17.8 psf
110 mph	C	56.9 psf	33.7 psf	25.8 psf	21.5 psf

2. Pressures are calculated assuming the fence is not located on the upper portion of a hill or escarpment.
3. End pressures are calculated assuming a minimum 270 ft. long fence with no corners.

From this chart it can be observed that most installations of the RhinoRock fence panel will be adequate in a 120 mph exposure B, or 100 mph exposure C wind. Installations at the top of hill or escarpment or in areas where the wind speed or exposure are higher than shown may be possible depending on the configuration of the fence. The presence of a corner near the free end of a fence may possibly reduce the significant end pressures that develop. We recommend that each fence installation be evaluated by a qualified structural engineer on a case by case basis.

Please call if you have questions.

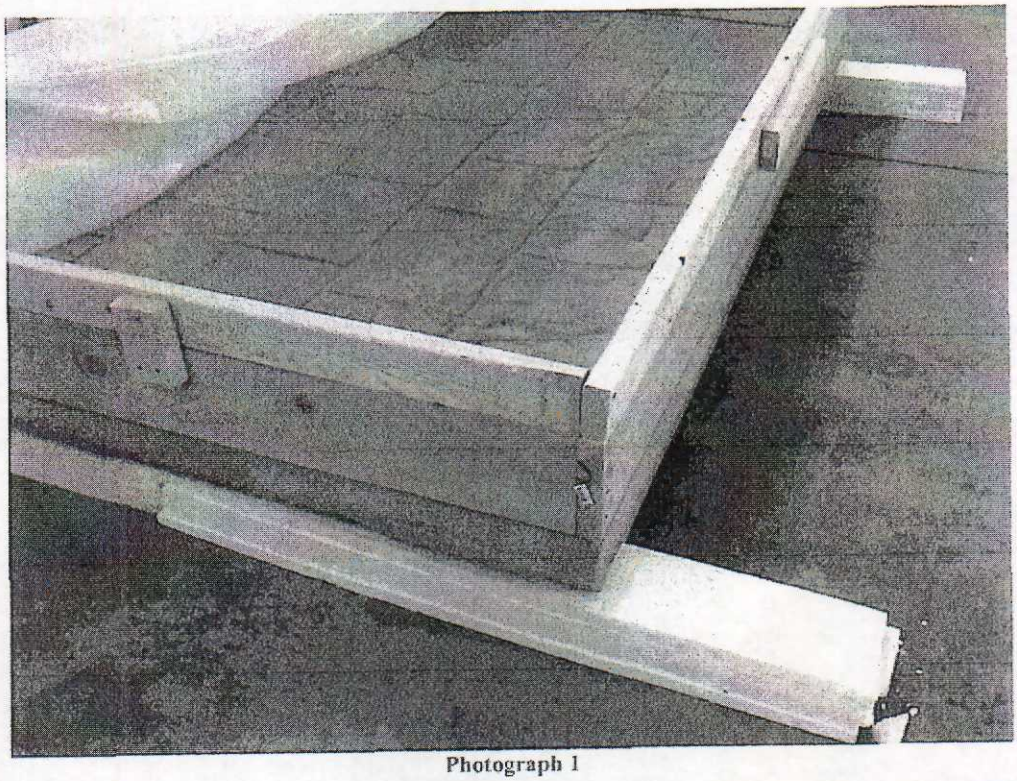
Sincerely,

Daniel D. Goodrich, S.E.

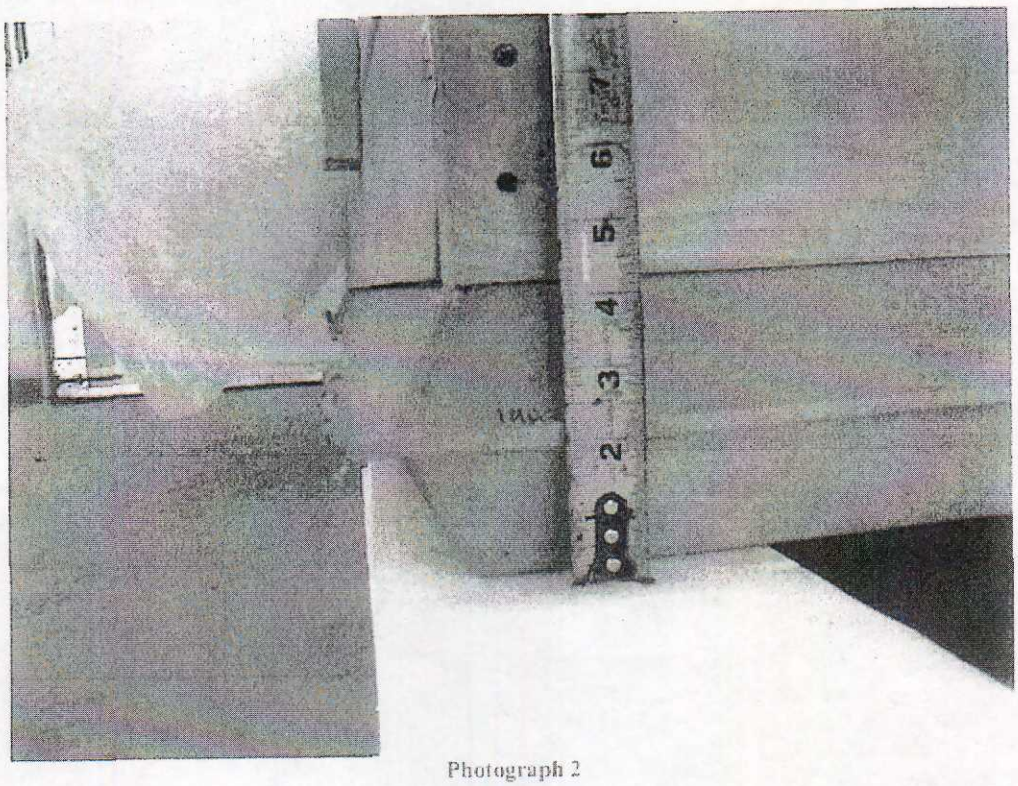
Reviewed,

Steven J. Cosper, S.E.

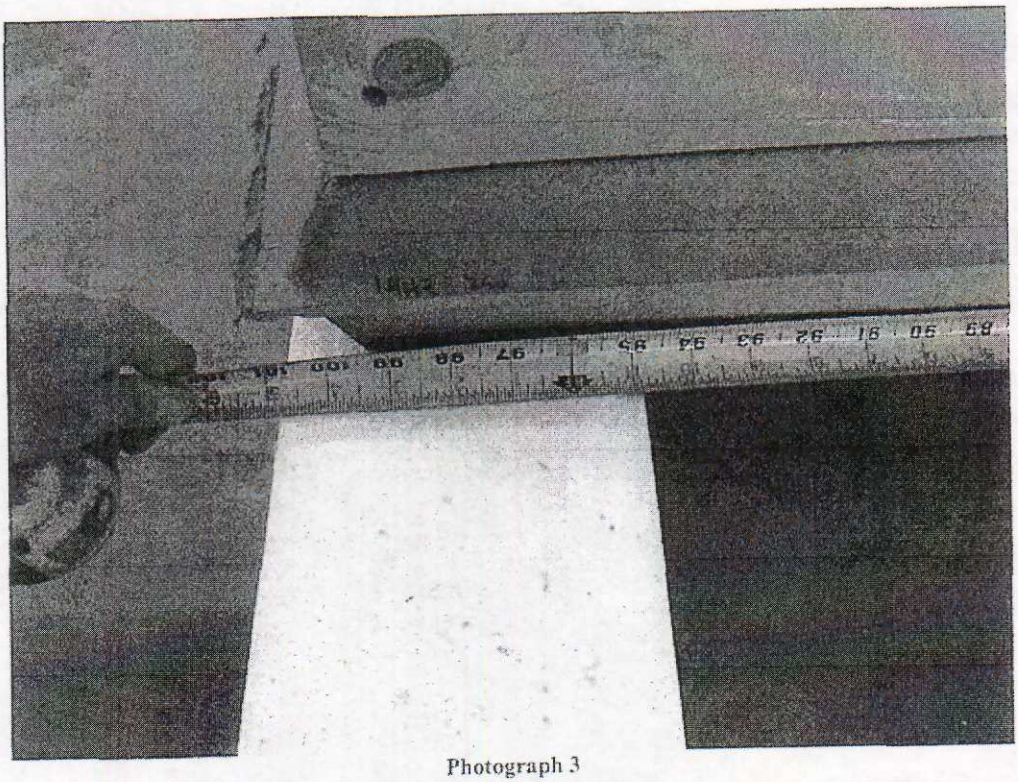
Encl.



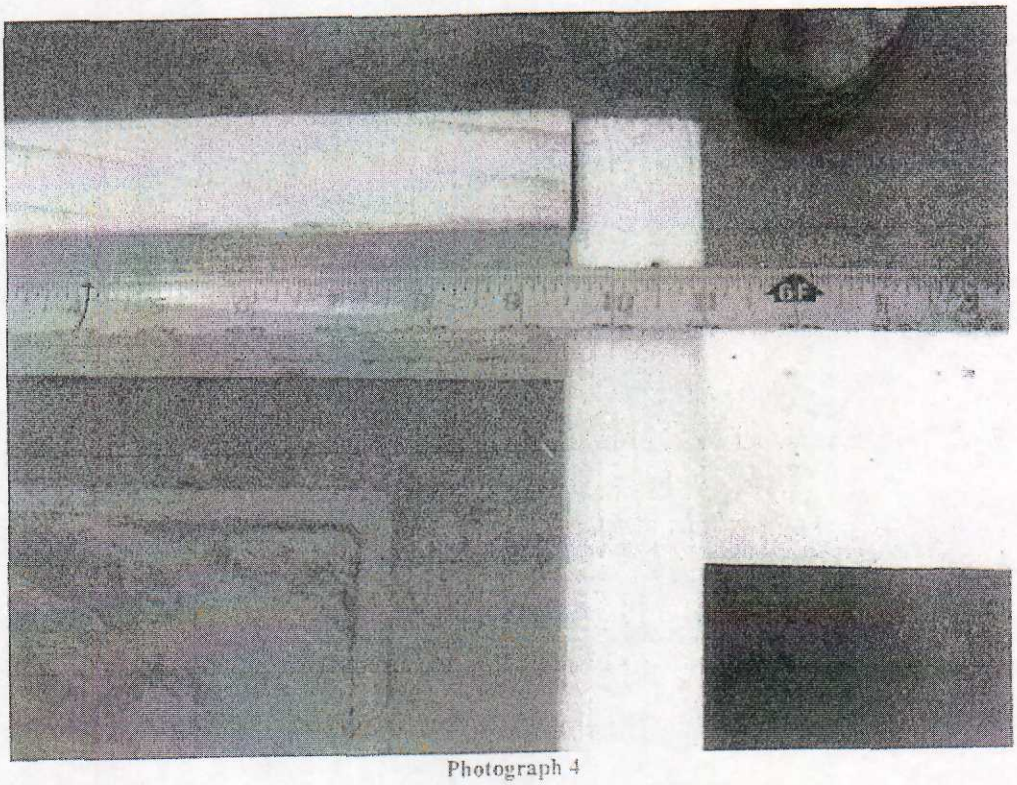
Photograph 1



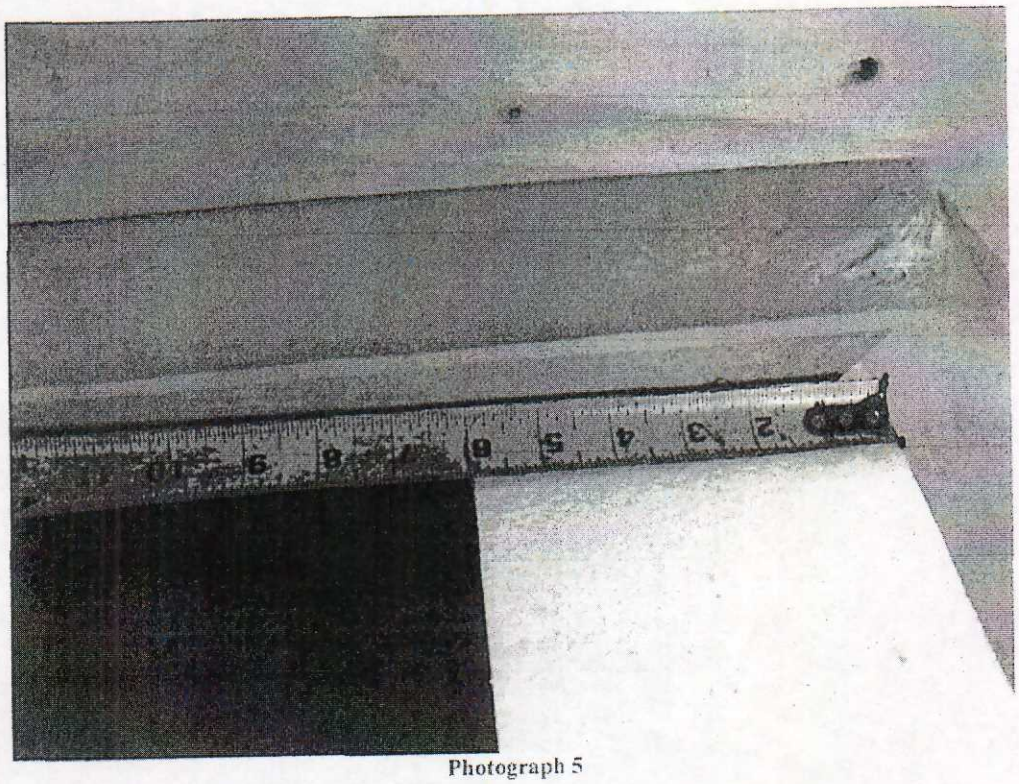
Photograph 2



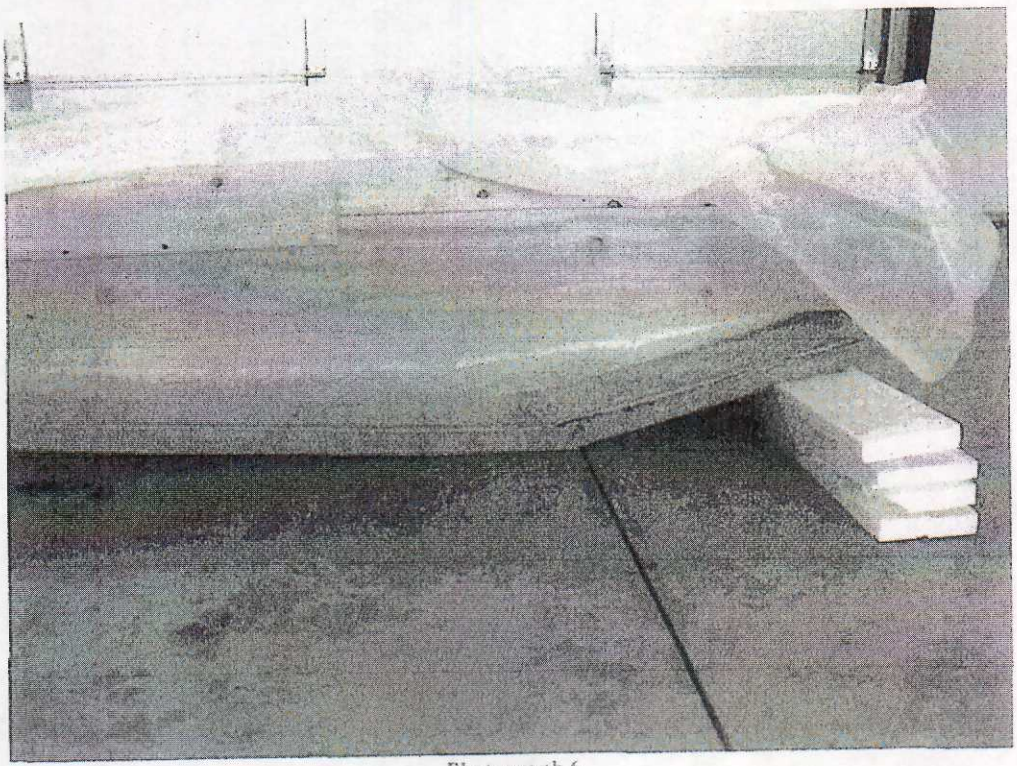
Photograph 3



Photograph 4



Photograph 5



Photograph 6

ASCE 7-05 Wind

Section 6.5.14 – Design Wind loads on solid freestanding walls

Project: Rhino Fence
Location:
Job: 9536

Step 1.	V =	90	Mph	← Wind speed
	K_d =	0.85	Table 6-4	
Step 2.	I =	0.87	Table 6-1	< Importance factor
Step 3.	Exp.	B	Section 6.5.6	← Exposure
	Wall height h =	6	(ft)	
	K_h =	0.57	Table 6-3	
Step 4.	K_{zt} =	1	Figure 6-4	← No Hill or Escarpment
Step 5.	G =	0.85	Section 6.5.8	
Step 9.	q_h =	8.8	psf	Cp varies with aspect ratio of fence
Step 10.	F =	7.5	* C_f * As	

Case A & B

C_f = 1.3

F = 9.74 psf ← Interior pressure

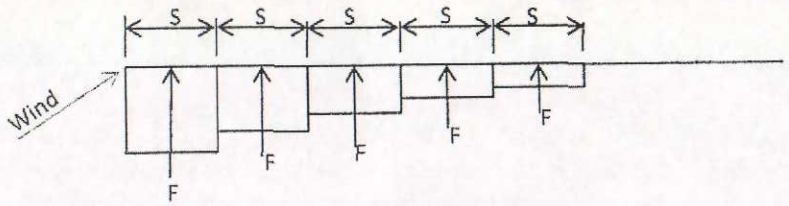
Use 10 psf minimum.

Case C

		Reduction Factor	Modified C_f	Final Wall Pressure	
0 to S	4.3	0.8	3.44	**25.8**	psf
S to 2S	2.55	0.8	2.04	**15.3**	psf
2S to 3S	1.95	0.8	1.56	**11.7**	psf
3S to 4S	1.85	0.8	1.48	**11.1**	psf
4S to 5S	1.85	0.8	1.48	**11.1**	psf
5S to 10S	1.1	0.8	0.88	**6.6**	psf

← Max pressure @ fence ends.

Case C only controls at the ends of the fence. Case A & B control for interior portions.



ASCE 7-05 Wind

Section 6.5.14 – Design Wind loads on solid freestanding walls

Project: Rhino Fence
Location:
Job: 9536

Step 1.	V =	100	Mph
	K_d =	0.85	Table 6-4
Step 2.	I =	0.87	Table 6-1
Step 3.	Exp.	B	Section 6.5.6
	Wall height h =	6	(ft)
	K_h =	0.57	Table 6-3
Step 4.	K_{zt} =	1	Figure 6-4
Step 5	G =	0.85	Section 6.5.8
Step 9.	q_h =	10.9	psf
Step 10.	F =	9.2	* C_f * As

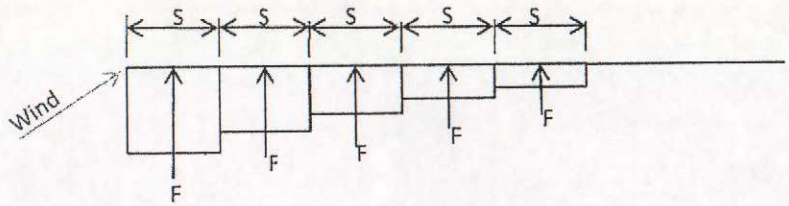
Case A & B

C_f =	1.3		
F =	12.02	psf	**Use 10 psf minimum.**

Case C

		Reduction Factor	Modified C_f	Final Wall Pressure	
0 to S	4.3	0.8	3.44	**31.8**	psf
S to 2S	2.55	0.8	2.04	**18.9**	psf
2S to 3S	1.95	0.8	1.56	**14.4**	psf
3S to 4S	1.85	0.8	1.48	**13.7**	psf
4S to 5S	1.85	0.8	1.48	**13.7**	psf
5S to 10S	1.1	0.8	0.88	**8.1**	psf

Case C only controls at the ends of the fence. Case A & B control for interior portions.



ASCE 7-05 Wind

Section 6.5.14 – Design Wind loads on solid freestanding walls

Project: Rhino Fence
Location:
Job: 9536

Step 1.	V =	110	Mph	
	K_d =	0.85	Table 6-4	
Step 2.	I =	0.87	Table 6-1	
Step 3.	Exp.	B	Section 6.5.6	
	Wall height h =	6	(ft)	
	K_h =	0.57	Table 6-3	
Step 4.	K_{zt} =	1	Figure 6-4	
Step 5.	G =	0.85	Section 6.5.8	
Step 9.	q_h =	13.2	psf	
Step 10.	F =	11.2	* C_f * As	

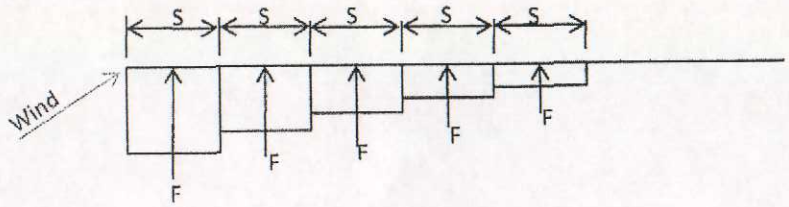
Case A & B

C_f =	1.3		
F =	14.55	psf	**Use 10 psf minimum.**

Case C

		Reduction Factor	Modified C_f	Final Wall Pressure	
0 to S	4.3	0.8	3.44	**38.5**	psf
S to 2S	2.55	0.8	2.04	**22.8**	psf
2S to 3S	1.95	0.8	1.56	**17.5**	psf
3S to 4S	1.85	0.8	1.48	**16.6**	psf
4S to 5S	1.85	0.8	1.48	**16.6**	psf
5S to 10S	1.1	0.8	0.88	**9.8**	psf

Case C only controls at the ends of the fence. Case A & B control for interior portions.



ASCE 7-05 Wind

Section 6.5.14 – Design Wind loads on solid freestanding walls

Project: Rhino Fence
Location:
Job: 9536

Step 1.	V =	120	Mph	
	K_d =	0.85	Table 6-4	
Step 2.	I =	0.87	Table 6-1	
Step 3	Exp.	B	Section 6.5.6	
	Wall height h =	6	(ft)	
	K_h =	0.57	Table 6-3	
Step 4.	K_{zt} =	1	Figure 6-4	
Step 5.	G =	0.85	Section 6.5.8	
Step 9.	q_h =	15.7	psf	
Step 10.	F =	13.3	* C_f * As	

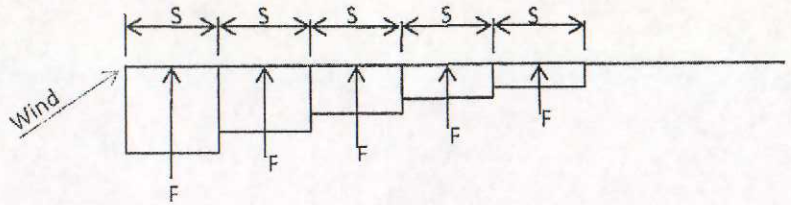
Case A & B

C_f =	1.3		
F =	17.31	psf	**Use 10 psf minimum.**

Case C

		Reduction Factor	Modified C_f	Final Wall Pressure	
0 to S	4.3	0.8	3.44	**45.8**	psf
S to 2S	2.55	0.8	2.04	**27.2**	psf
2S to 3S	1.95	0.8	1.56	**20.8**	psf
3S to 4S	1.85	0.8	1.48	**19.7**	psf
4S to 5S	1.85	0.8	1.48	**19.7**	psf
5S to 10S	1.1	0.8	0.88	**11.7**	psf

Case C only controls at the ends of the fence. Case A & B control for interior portions.



ASCE 7-05 Wind

Section 6.5.14 – Design Wind loads on solid freestanding walls

Project: Rhino Fence
Location:
Job: 9536

Step 1.	V =	90	Mph
	K_d =	0.85	Table 6-4
Step 2.	I =	0.87	Table 6-1
Step 3.	Exp.	C	Section 6.5.6
	Wall height h =	6	(ft)
	K_h =	0.85	Table 6-3
Step 4.	K_{zt} =	1	Figure 6-4
Step 5.	G =	0.85	Section 6.5.8
Step 9.	q_h =	13.0	psf
Step 10.	F =	11.1	* C_f * As

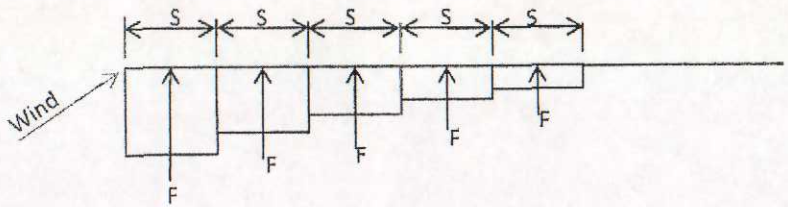
Case A & B

C_f =	1.3		
F =	14.38	psf	**Use 10 psf minimum.**

Case C

		Reduction Factor	Modified C_f	Final Wall Pressure	
0 to S	4.3	0.8	3.44	**38.1**	psf
S to 2S	2.55	0.8	2.04	**22.6**	psf
2S to 3S	1.95	0.8	1.56	**17.3**	psf
3S to 4S	1.85	0.8	1.48	**16.4**	psf
4S to 5S	1.85	0.8	1.48	**16.4**	psf
5S to 10S	1.1	0.8	0.88	**9.7**	psf

Case C only controls at the ends of the fence. Case A & B control for interior portions.



ASCE 7-05 Wind

Section 6.5.14 – Design Wind loads on solid freestanding walls

Project: Rhino Fence
Location:
Job: 9536

Step 1.	V =	100	Mph	
	K_d =	0.85	Table 6-4	
Step 2.	I =	0.87	Table 6-1	
Step 3.	Exp.	C	Section 6.5.6	
	Wall height h =	*6*	*(ft)*	
	K_h =	0.85	Table 6-3	
Step 4.	K_{zt} =	1	Figure 6-4	
Step 5.	G =	0.85	Section 6.5.8	
Step 9.	q_h =	16.1	psf	
Step 10.	F =	13.7	* C_f * As	

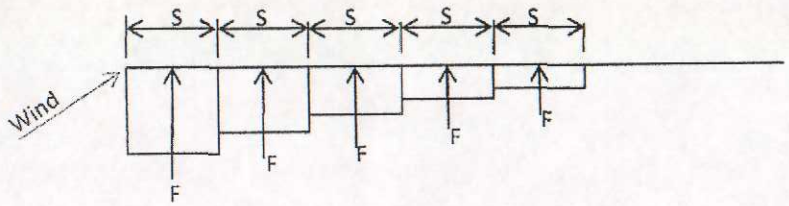
Case A & B

C_f =	1.3		
F =	17.76	psf	**Use 10 psf minimum.**

Case C

		Reduction Factor	Modified C_f	Final Wall Pressure	
0 to S	4.3	0.8	3.44	**47.0**	psf
S to 2S	2.55	0.8	2.04	**27.9**	psf
2S to 3S	1.95	0.8	1.56	**21.3**	psf
3S to 4S	1.85	0.8	1.48	**20.2**	psf
4S to 5S	1.85	0.8	1.48	**20.2**	psf
5S to 10S	1.1	0.8	0.88	**12.0**	psf

Case C only controls at the ends of the fence. Case A & B control for interior portions.



ASCE 7-05 Wind

Section 6.5.14 – Design Wind loads on solid freestanding walls

Project: Rhino Fence
Location:
Job: 9536

Step 1.	V =	110	Mph	
	K_d =	0.85	Table 6-4	
Step 2.	I =	0.87	Table 6-1	
Step 3.	Exp.	C	Section 6.5.6	
	Wall height h =	6	(ft)	
	K_h =	0.85	Table 6-3	
Step 4.	K_{zt} =	1	Figure 6-4	
Step 5.	G =	0.85	Section 6.5.8	
Step 9.	q_h =	19.4	psf	
Step 10.	F =	16.5	* C_f * As	

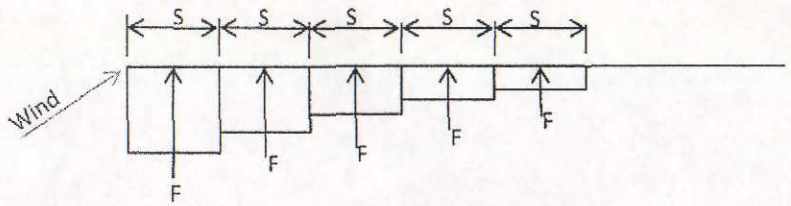
Case A & B

C_f =	1.3		
F =	21.49	psf	**Use 10 psf minimum.**

Case C

		Reduction Factor	Modified C_f	Final Wall Pressure	
0 to S	4.3	0.8	3.44	**56.9**	psf
S to 2S	2.55	0.8	2.04	**33.7**	psf
2S to 3S	1.95	0.8	1.56	**25.8**	psf
3S to 4S	1.85	0.8	1.48	**24.5**	psf
4S to 5S	1.85	0.8	1.48	**24.5**	psf
5S to 10S	1.1	0.8	0.88	**14.5**	psf

Case C only controls at the ends of the fence. Case A & B control for interior portions.



Riverton City Council

April 7, 2015

OQUIRRH HILLS middle school

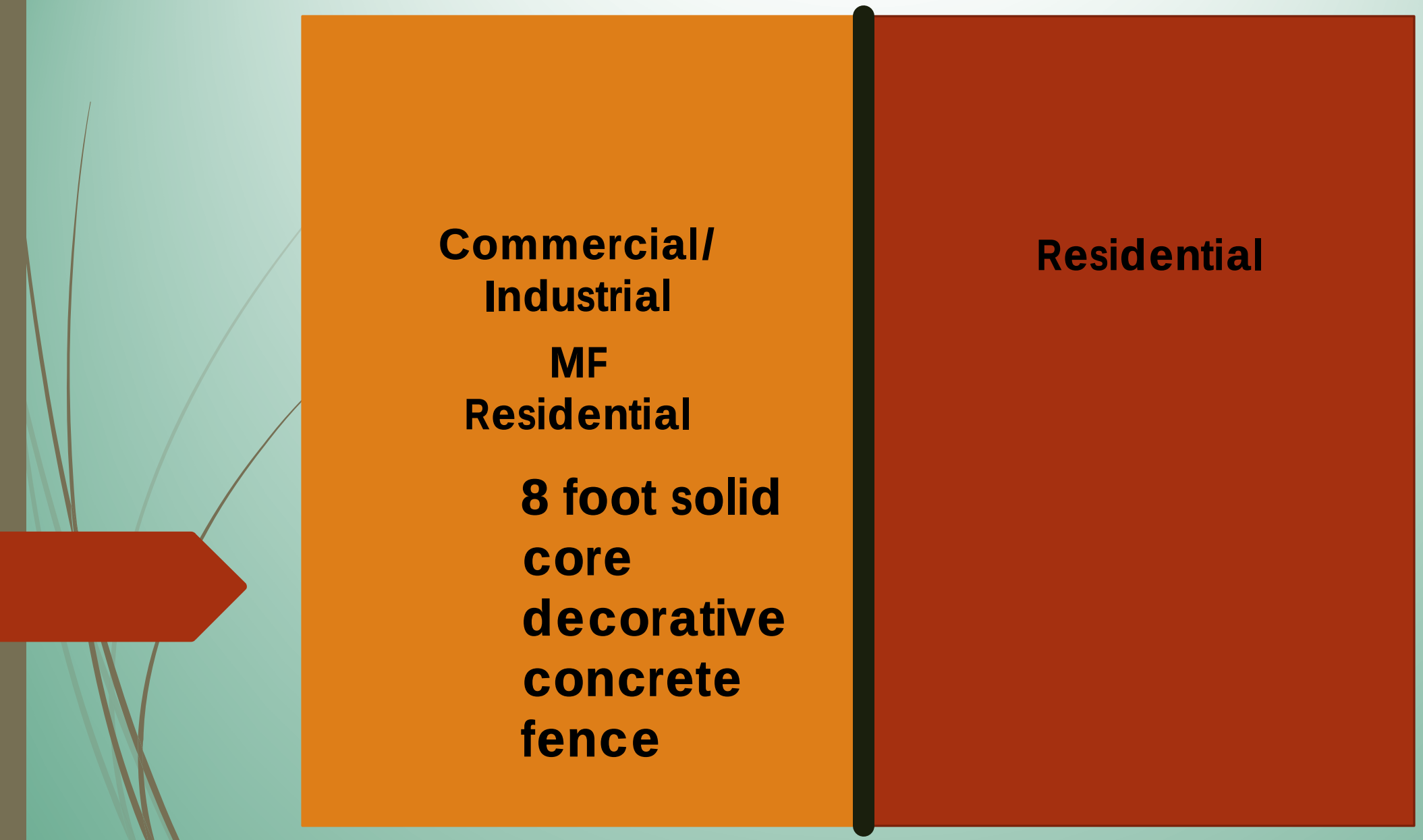
12949 South 2700 West

Principal: Michael Glenn

Fencing Ordinance

Fencing Ordinance - Proposed

- **18.155.080 Noncompatible Zones.**
- (1) Noncompatible Zones. A solid core decorative concrete fence with a minimum height of six feet shall be required between noncompatible zones. Both sides of the fence shall receive equal treatment with respect to pattern, color, etc. Hollow, foam core, fiberglass/concrete mix, or other alternative fence types are not permitted.
- (2) Fencing Height. Fencing shall be a minimum of eight (8) feet in height between commercial/industrial zones and residential zoning of any type, and between multi-family development and single family residential zones


Commercial/
Industrial
MF
Residential
8 foot solid
core
decorative
concrete
fence
Residential

Residential Development

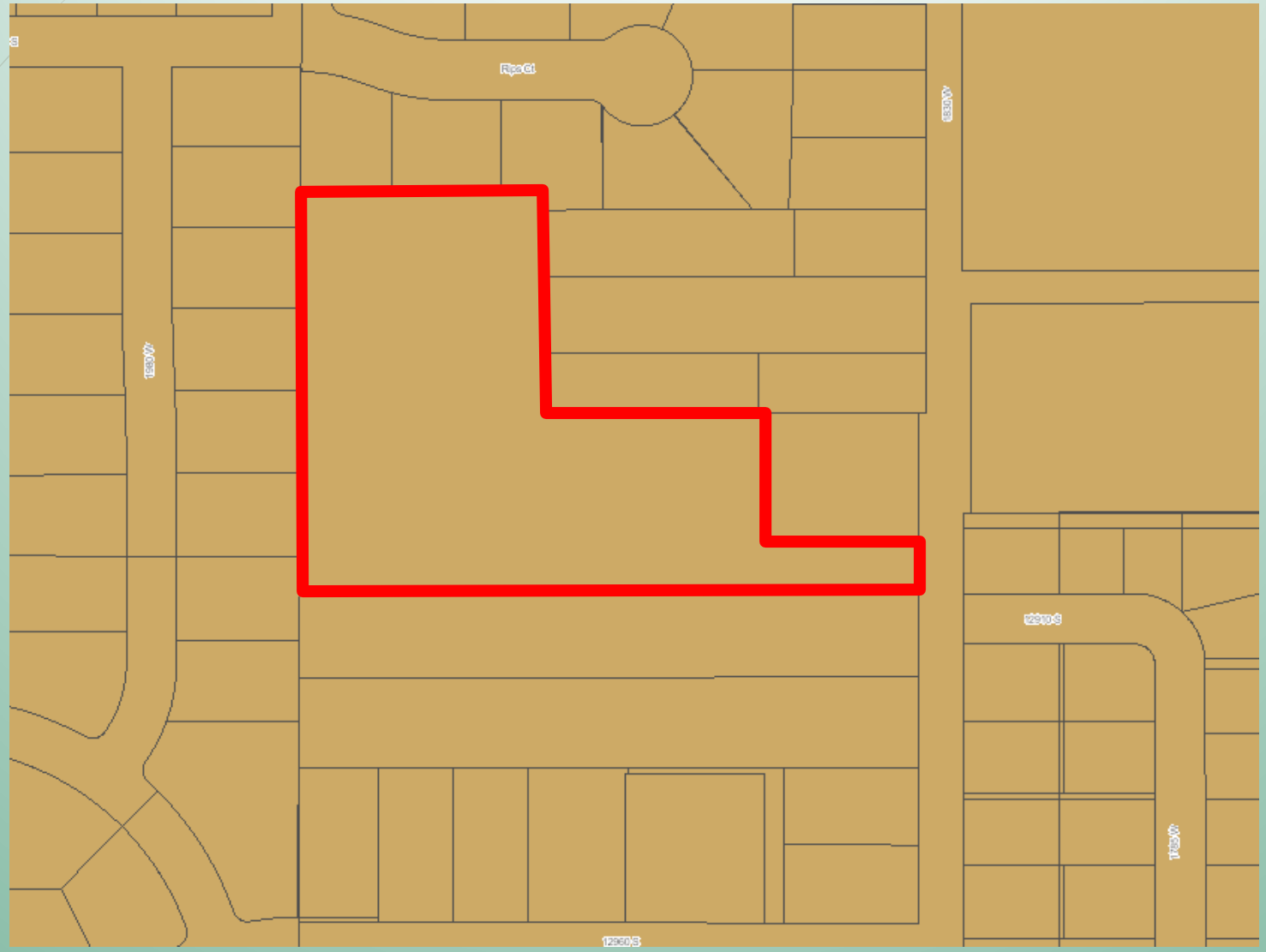
6 foot solid core decorative concrete fence

Residential With Animal Rights

Perimeter Fencing

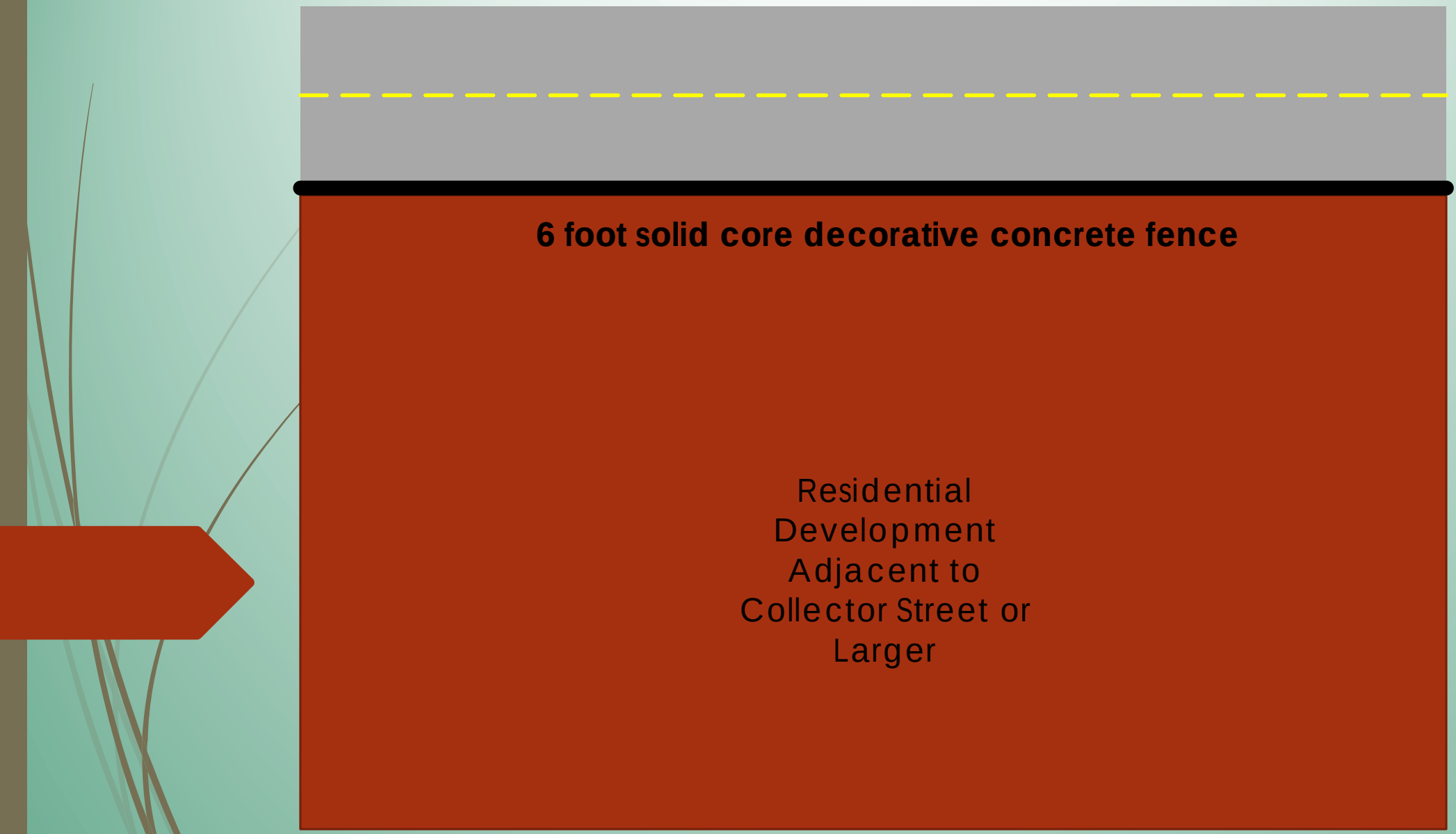
- **18.155.090 Fences surrounding development.**
- (1) Developments Adjacent to Compatible Zones. New development adjacent to compatible zones shall have a solid fence or wall at a minimum height of six (6) feet. Fencing shall be consistent in color and design with area fencing, and shall be reviewed as part of development approvals. The Planning Commission and City Council may require fence type and design based on surrounding fencing. Fencing for all subdivisions shall meet all ordinances as outlined in Chapter 17.15 RCC.

Perimeter Fencing



Collector Street Fencing - Proposed

- (2) Collector/Arterial Street Fencing. Fencing along collector and arterial streets as defined by Riverton City shall consist of a minimum six (6) feet high decorative solid core concrete fencing. Hollow, foam core, fiberglass/concrete mix, or other alternative fence types are not permitted. Both sides of the fence shall receive equal treatment with respect to pattern, color, etc.


6 foot solid core decorative concrete fence
Residential
Development
Adjacent to
Collector Street or
Larger

Ditches/Waterways- Proposed

- (4) Irrigation Fencing. Fencing along ditches, canals or other irrigation lines shall consist of a minimum six (6) feet high decorative solid core concrete fencing. Hollow, foam core, fiberglass/concrete mix, or other alternative fence types are not permitted. Both sides of the fence shall receive equal treatment with respect to pattern, color, etc.

Development

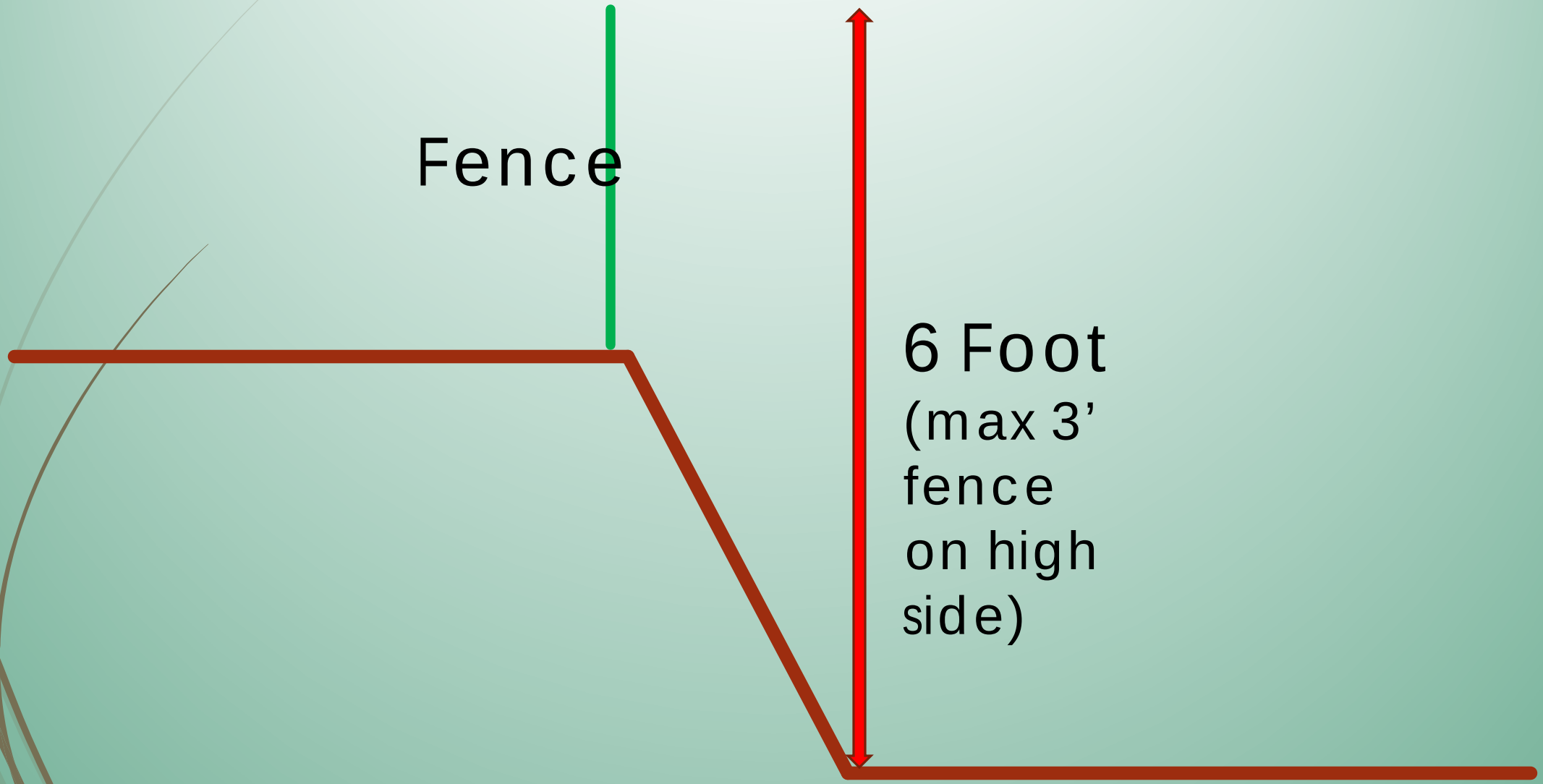
6 foot solid core decorative concrete fence

Ditches, Canals, or Other Waterways

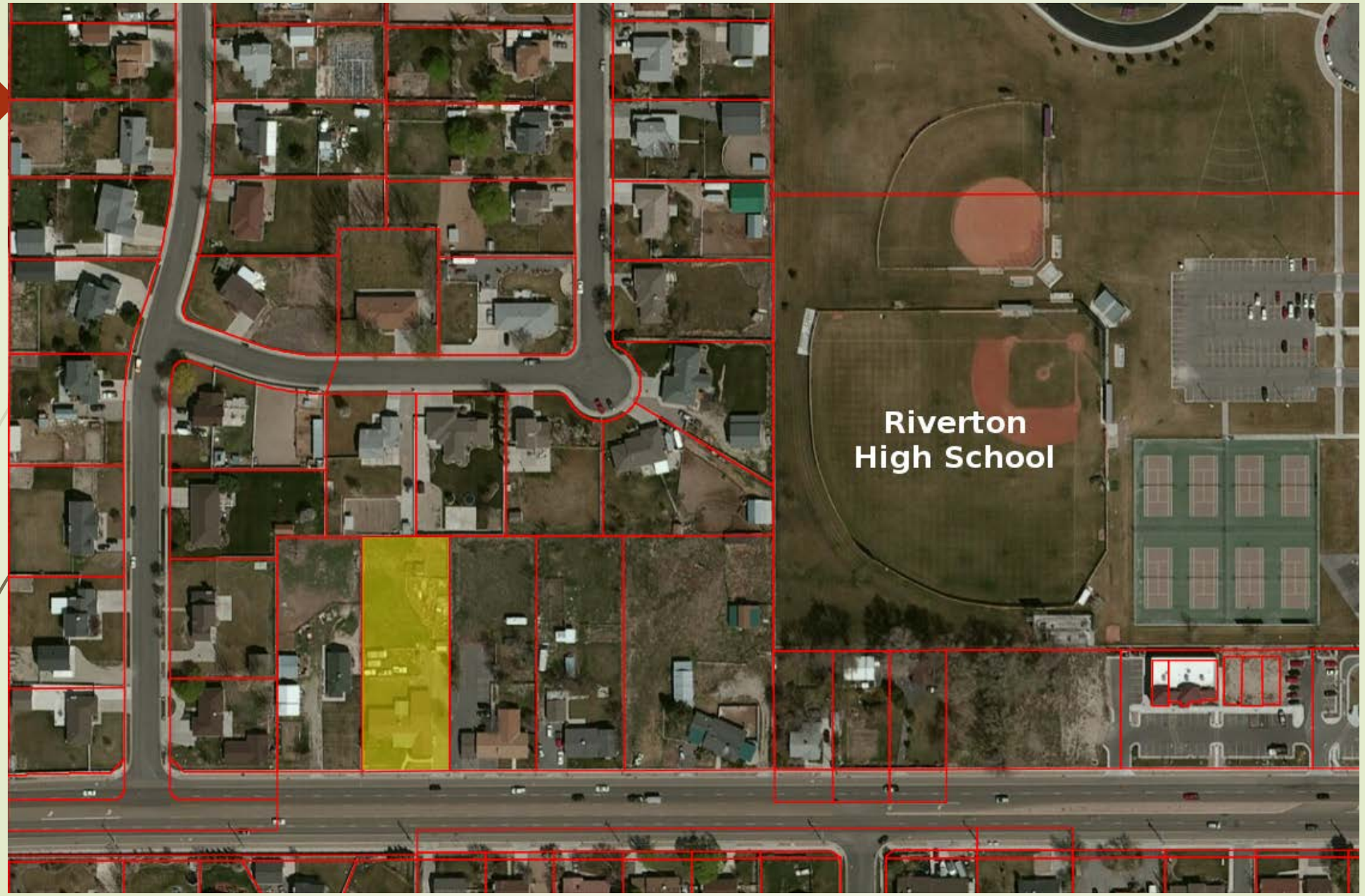
Elevation Differential

- 1) Change in Elevation. Fences, walls, or hedges located along a property line separating two lots where there is a difference in the grade of two feet or greater shall be approved by the Planning Manager prior to installation, and may require Engineering Department review and approval.

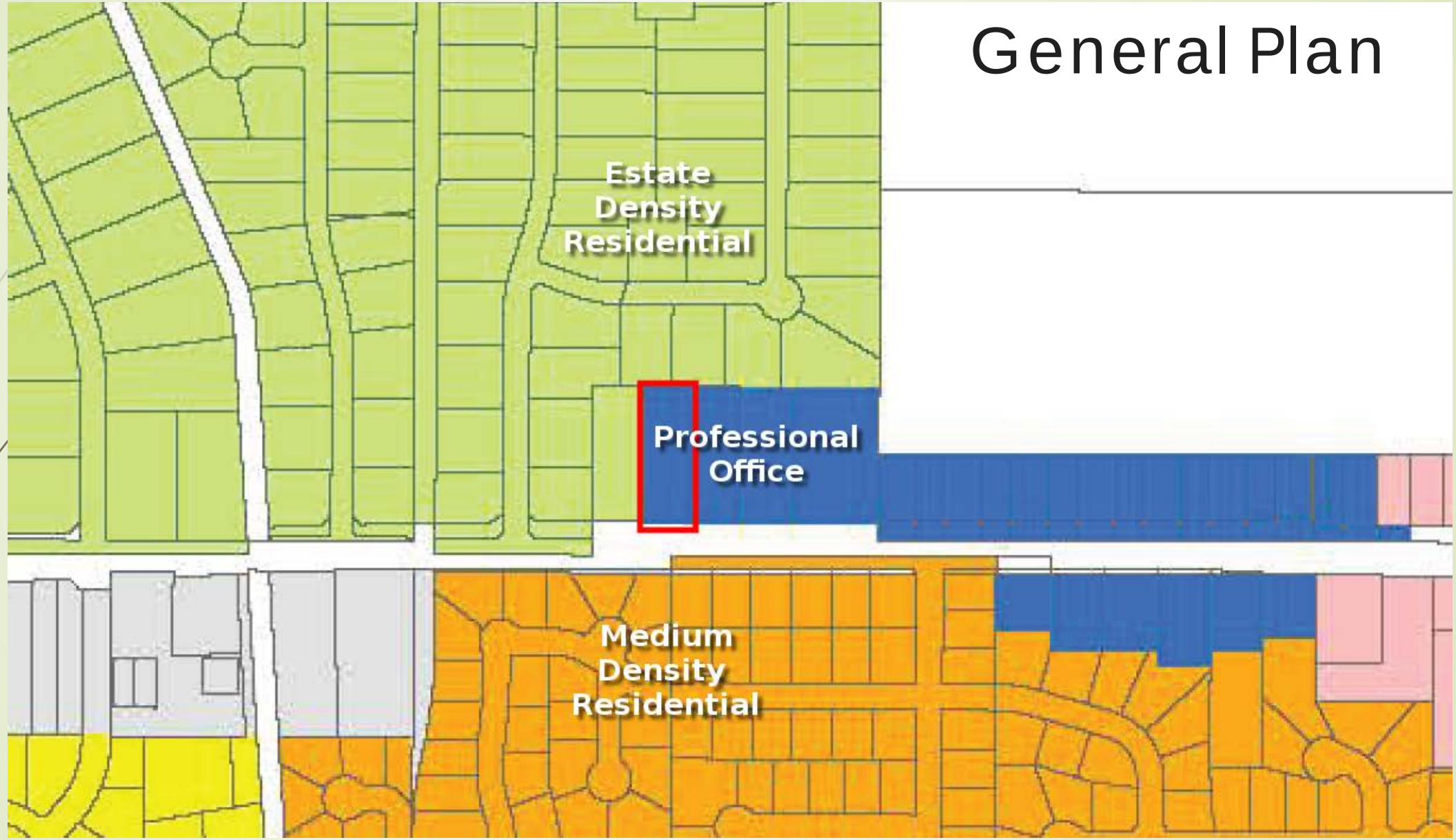
Elevation Differential

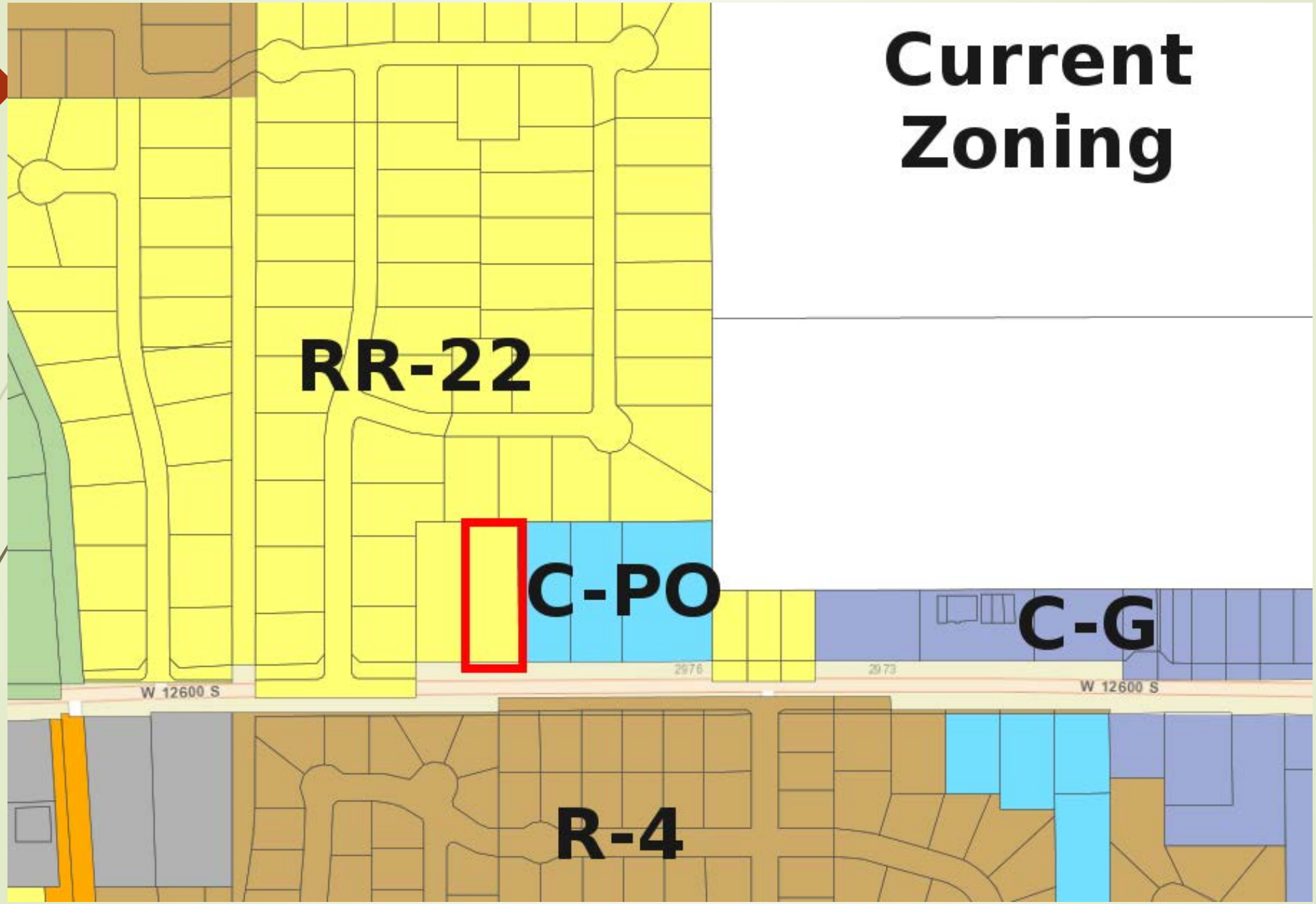


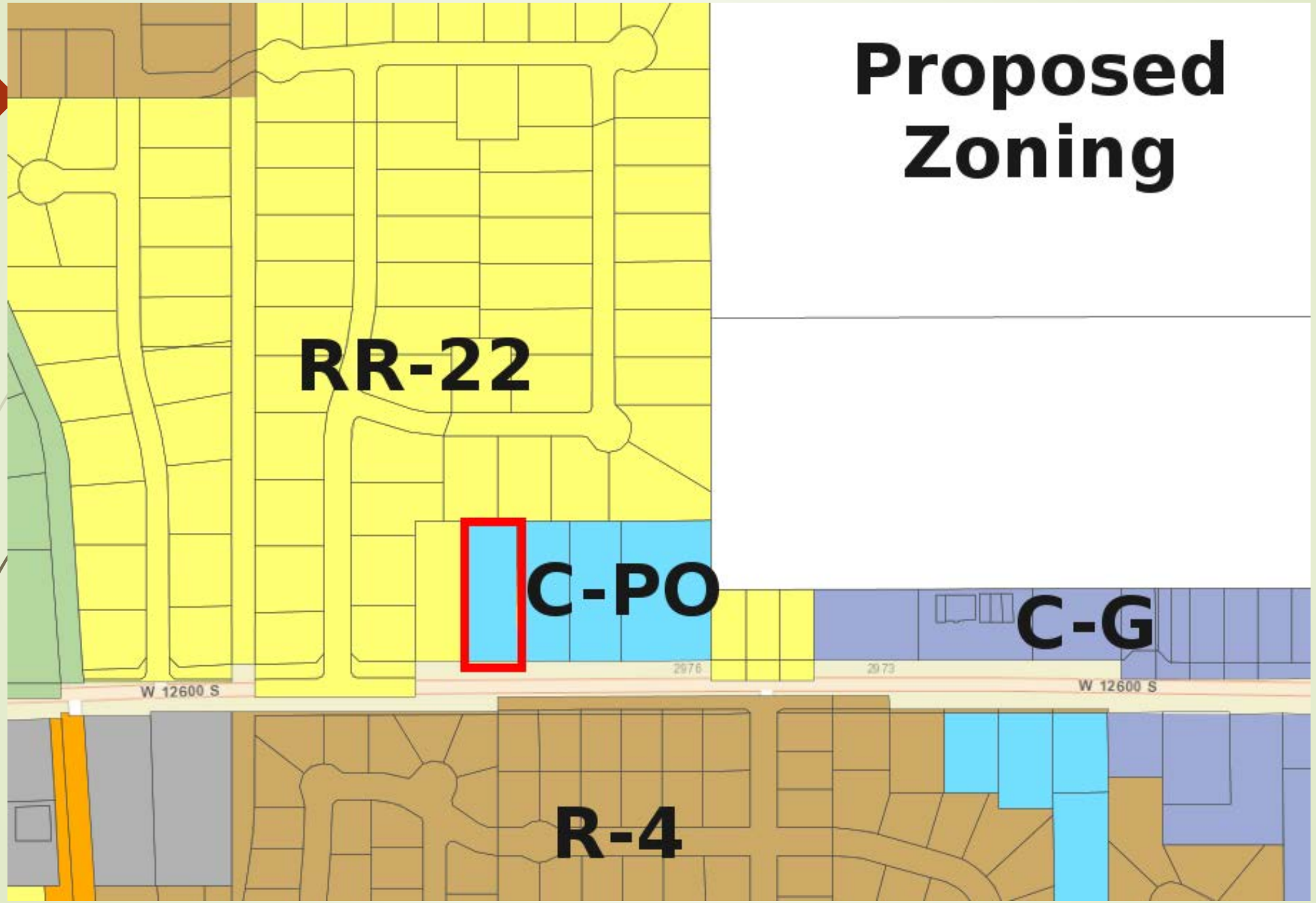
Pritzkau Rezone


Riverton
High School

General Plan




Current Zoning
RR-22
C-PO
C-G
R-4
W 12600 S
W 12600 S
2976
2973


Proposed Zoning
RR-22
C-PO
C-G
R-4
W 12600 S
W 12600 S
2976
2973

Riverton City Council

April 7, 2015